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U.S. PATENT APPLICATION

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Invention:

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AIRFOIL SHAPE FOR A TURBINE BUCKET

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AIRFOIL SHAPE FOR A TURBINE BUCKET

· BACKGROUND OF THE INVENTION

[0001] The present invention relates to an airfoil for a bucket of a stage of a gas turbine and particularly relates to a first stage turbine bucket airfoil profile.

[0002] Many system requirements must be met for each stage of the hot gas path section of a gas turbine in order to meet design goals including overall improved efficiency and airfoil loading. Particularly, the buckets of the first stage of the turbine section must meet the thermal and mechanical operating requirements for that particular stage.

BRIEF DESCRIPTION OF THE INVENTION

[0003] In accordance with the preferred embodiment of the present invention there is provided a unique airfoil shape for a bucket of a gas turbine, preferably the first stage bucket, that enhances the performance of the gas turbine. The present airfoil shape is a modification of a prior airfoil design. Specifically, by reshaping the trailing edge from the prior known design, the present airfoil is unique and not a direct scale of the prior known bucket airfoils. More specifically, cutbacks are applied to the trailing edge of the prior known design, particularly along its entire length, affording a wholly new overall airfoil profile.

[0004] The bucket airfoil profile hereof is defined by a unique loci of points to achieve the necessary

efficiency, and loading requirements. These unique loci of points define the nominal airfoil profile and are identified by the X, Y and Z Cartesian coordinates of Table I which follows. The 1000 points for the coordinate values shown in Table I are relative to the turbine centerline and for a cold, i.e., room temperature bucket at various cross-sections of the bucket airfoil along its length. The positive X, Y and Z directions are axial toward the exhaust end of the turbine, tangential direction of engine rotation and radially the outwardly toward the bucket tip, respectively. The X and Y coordinates are given in distance dimensions, e.g., units of inches, and are joined smoothly at each Z location to form smooth continuous cross-section. coordinates are given non-dimensionalized form from 0.05 (5%) span to 0.95 (95%) span. By multiplying the airfoil height dimension, e.g., in inches, by the non-dimensional Z value of Table I, the airfoil shape, i.e., the profile, of the bucket airfoil is obtained. Each defined airfoil section in the X, Y plane is joined smoothly with adjacent airfoil sections in the Z direction to form the complete airfoil The resulting airfoil particularly has a trailing edge cutback as compared with a prior known bucket.

[0005] It will be appreciated that as each bucket airfoil heats up in use, the profile will change as a result of mechanical loading and temperature. Thus, the cold or room temperature profile is given by the X, Y and Z coordinates for manufacturing purposes. Because a manufactured bucket airfoil profile may be different from the nominal airfoil profile given by the following table, a distance of plus or minus 0.150 inches from the nominal

profile in a direction normal to any surface location along the nominal profile and which includes any coating, defines a profile envelope for this bucket airfoil. The airfoil shape is robust to this variation without impairment of the mechanical and aerodynamic functions of the bucket.

[0006] It will also be appreciated that the airfoil can scaled up or scaled down geometrically introduction into similar turbine designs. Consequently, the X and Y coordinates in inches and the non-dimensional Z coordinates, when converted to inches, of the nominal airfoil profile given below may be a function of the same constant or number. That is, the X and Y coordinate values in inches, and optionally the Z coordinate values when converted to inches, may be multiplied or divided by the same constant or number to provide a scaled up or scaled down version of the bucket airfoil profile while retaining the airfoil section shape.

[0007] a preferred embodiment according to present invention, there is provided a turbine bucket including a bucket airfoil having an airfoil shape, the airfoil having a nominal profile substantially in accordance with Cartesian coordinate values of X, Y and Z forth in Table wherein the Z values set I non-dimensional values from 0.05 span to 0.95 convertible to Z distances in inches by multiplying the Z values by a height of the airfoil in inches, and wherein X and Y are distances in inches which, when connected by smooth continuing arcs, define airfoil profile sections at each distance Z, the profile sections at the Z distances being joined smoothly with one another to form a complete airfoil shape.

In a further preferred embodiment according to [8000] the present invention, there is provided a turbine bucket including a bucket airfoil having an uncoated nominal airfoil profile substantially in accordance Cartesian coordinate values of X, Y and Z set forth in Table I wherein the Z values are non-dimensional values from 0.05 span to 0.95 span convertible to Z distances in inches by multiplying the Z values by a height of the airfoil in inches, and wherein X and Y are distances in inches which, when connected by smooth continuing arcs, define airfoil profile sections at each Z distance, the profile sections at the Z distances being joined smoothly with one another to form a complete airfoil shape, the X and Y distances being scalable as a function of the same constant or number to provide a scaled-up or scaled-down airfoil.

[0009] In a further preferred embodiment according to the present invention, there is provided a turbine comprising a turbine wheel having a plurality of buckets, each of the buckets including an airfoil having an airfoil shape, the airfoil having a nominal profile substantially in accordance with Cartesian coordinate values of X, Y and Z set forth in Table I wherein the Z values are non-dimensional values from 0.05 span to 0.95 span convertible to Z distances in inches by multiplying the Z values by a height of the airfoil in inches, and wherein X and Y are distances in inches which, when connected by smooth continuing arcs, define the airfoil profile sections at each distance Z, the profile sections

at the Z distances being joined smoothly with one another to form a complete airfoil shape.

[0010] In a further preferred embodiment according to the present invention, there is provided a turbine comprising a turbine wheel having a plurality of buckets, the buckets including an airfoil having profile substantially uncoated nominal airfoil accordance with Cartesian coordinate values of X, Y and Z in Table Ι wherein the Z values set forth from 0.05span to 0.95 non-dimensional values convertible to Z distances in inches by multiplying the Z values by a height of the airfoil in inches, and wherein X and Y are distances in inches which, when connected by smooth continuing arcs, define airfoil profile sections at each distance Z, the profile sections at the Z distances being joined smoothly with one another to form a complete airfoil shape, the X, Y and Z distances being scalable as a function of the same constant or number to provide a scaled-up or scaled-down bucket airfoil.

BRIEF DESCRIPTION OF THE DRAWINGS

[0011] FIGURE 1 is a schematic representation of a hot gas path through multiple stages of a gas turbine and illustrates a first stage bucket airfoil according to a preferred embodiment of the present invention;

[0012] FIGURE 2 is a perspective view of the bucket according to a preferred embodiment of the present invention with the bucket airfoil illustrated in conjunction with its platform, shank and near-axial entry dovetail connection;

[0013] FIGURE 3 is a side elevational view of the bucket of Figure 2;

[0014] FIGURE 4 is an opposite side elevational view thereof;

[0015] FIGURES 5 and 6 are respective opposite end views of the bucket as viewed from the leading and trailing edges of the airfoil;

[0016] FIGURE 7 is a top plan view looking radially inwardly from the tip of the bucket;

[0017] FIGURE 8 is a representative airfoil profile section taken generally about a mid-span portion of the airfoil hereof;

[0018] FIGURE 9 is a schematic representation illustrating a trailing edge reduction for comparison purposes with a prior known bucket airfoil; and

[0019] FIGURE 10 is a schematic illustration of the trailing edge diameter of the bucket airfoil hereof illustrating its configuration in relation to the prior known bucket.

DETAILED DESCRIPTION OF THE INVENTION

[0020] Referring now to the drawings, particularly to Figure 1, there is illustrated a hot gas path, generally designated 10, of a gas turbine 12 including a plurality of turbine stages. Three stages are illustrated. For example, the first stage comprises a plurality of

circumferentially spaced nozzles 14 and buckets 16. The nozzles are circumferentially spaced one from the other and fixed about the axis of the rotor. The first stage buckets 16, of course, are mounted on the turbine rotor A second stage of the turbine 12 illustrated, including a plurality of circumferentially spaced nozzles 18 and a plurality of circumferentially spaced buckets 20 mounted on the rotor 17. The third stage is also illustrated including a plurality of circumferentially spaced nozzles 22 and buckets mounted on rotor 17. It will be appreciated that the nozzles and buckets lie in the hot gas path 10 of the turbine, the direction of flow of the hot gas through the hot gas path 10 being indicated by the arrow 26.

[0021] It will be appreciated that the buckets, for example, the buckets 16 of the first stage are mounted on a rotor wheel 19 forming part of rotor 17. Each bucket 16 is provided, as illustrated in Figures 2 and 3, with a platform 30, a shank 32 and an axial dovetail 34 for connection with a complementary-shaped mating dovetail, not shown, on the rotor wheel 19. It will also be appreciated that each bucket 16 has a bucket airfoil 36. Thus, each of the buckets 16 has a cross-sectional airfoil profile at any cross-section from the airfoil root 31 (Figure 3) at a midpoint of platform 30 to the bucket tip 33 in the shape of an airfoil

[0022] To define the airfoil shape of each first stage bucket airfoil, there is a unique set or loci of points in space that meet the stage requirements and can be manufactured. This unique loci of points meets the requirements for stage efficiency and reduced thermal and

mechanical stresses. The loci of points are arrived at by iteration between aerodynamic and mechanical loadings enabling the turbine to run in an efficient, safe and smooth manner. The loci which defines the bucket airfoil profile comprises a set of 1000 points relative to the axis of rotation of the turbine. A Cartesian coordinate system of X, Y and Z values given in Table 1 below defines the profile section of the bucket airfoil at various locations along its length. The coordinate values for the X and Y coordinates are set forth in inches in Table I although other units of dimensions may be used when the values are appropriately converted. I values are set forth in Table I in non-dimensional form from 0.05 (5%) span to 0.95 (95% span). To convert the Z value to a Z coordinate value, e.g., in inches, the non-dimensional Z value given in Table I is multiplied by the height of the airfoil 36 in inches. The Cartesian coordinate system has orthogonally-related X, Y and Z axes and the X axis lies parallel to the turbine rotor centerline, i.e., the rotary axis and a positive X coordinate value is axial toward the aft, i.e., exhaust end of the turbine. The positive Y coordinate value looking aft extends tangentially in the direction of rotation of the rotor and the positive Z coordinate value is generally radially outwardly toward the bucket tip.

[0023] By defining X and Y coordinate values at selected locations in a Z direction normal to the X, Y plane, the bucket airfoil profile section, e.g., profile section 40 of Figure 8, at each Z distance along the length of the airfoil can be ascertained. By connecting the X and Y values with smooth continuing arcs, each

profile section 40 at each distance Z is fixed. The airfoil profile sections 40 of the various surface locations between the distances Z are determined by smoothly connecting the adjacent profile sections to one another to form the entire airfoil profile. These values represent the airfoil profile sections at ambient, non-operating or non-hot conditions and are for an uncoated airfoil.

The Table I values for X and Y are generated and [0024] shown to four decimal places for determining the profile The fourth decimal place, however, is of the airfoil. not significant and may be rounded up or down. There are. typical manufacturing tolerances as well as coatings which must be accounted for in the actual profile of the airfoil. Accordingly, the values for the airfoil profile given in Table I are for a nominal airfoil. It will therefore be appreciated that ± typical manufacturing tolerances, i.e., \pm values, including any coating thicknesses, are additive to the X and Y values given in Table I below. Accordingly, a distance of \pm 0.150 inches in a direction normal to any surface location along the airfoil profile defines an airfoil profile envelope for this particular bucket airfoil design and turbine, i.e., a range of variation between measured points on the actual airfoil surface at nominal cold temperature and the ideal position of those points as given in the Table below at the same temperature. bucket airfoil design is robust to this range of variation without impairment of mechanical and aerodynamic functions.

[0025] The coordinate values given in Table I below provide the preferred nominal profile envelope.

	TABLE I	
τ X	Y	Z
Inches	Inches	% Span
-1.3594	-0.5213	0.05
-1.2754	-0.5233	0.05
-1.1942	-0.4993	0.05
-1.1157	-0.4673	0.05
-1.0376	-0.4344	0.05
-0.9588	-0.4030	0.05
-0.8792	-0.3740	0.05
-0.7987	-0.3474	0.05
-0.7176	-0.3227	0.05
-0.6361	-0.2995	0.05
-0.5541	-0.2782	0.05
-0.4715	-0.2592	0.05
-0.3883	-0.2431	0.05
-0.3045	-0.2302	0.05
-0.2202	-0.2208	0.05
-0.1357	-0.2155	0.05
-0.0509	-0.2144	0.05
0.0338	-0.2180	0.05
0.1181	-0.2264	0.05
0.2018	-0.2399	0.05
0.2845	-0.2583	0.05
0.3659	-0.2818	0.05
0.4458	-0.3101	0.05
0.5239 0.6000	-0.3430 -0.3804	0.05 0.05
0.6738	-0.4220	0.05
0.7453	-0.4675	0.05
0.7433	-0.5166	0.05
0.8810	-0.5691	0.05
0.9450	-0.6246	0.05
1.0066	-0.6829	0.05
1.0656	-0.7436	0.05
1.1223	-0.8067	0.05
1.1766	-0.8717	0.05
1.2287	-0.9386	0.05
1.2787	-1.0071	0.05
1.3272	-1.0766	0.05
1.3746	-1.1468	0.05
1.4284	-1.2110	0.05

X	Y	Z
Inches	Inches	% Span
1.5101	-1.2115	0.05
1.5576	-1.1449	0.05
1.5383 1.5074	-1.0633 -0.9843	0.05 0.05
1.4748	-0.9061	0.05
1.4417	-0.8280	0.05
1.4085	-0.7501	0.05
1.3750	-0.6722 -0.5944	0.05
1.3414 1.3074	-0.5944	0.05 0.05
1.2731	-0.4392	0.05
1.2383	-0.3619	0.05
1.2030	-0.2849	0.05
1.1671	-0.2081 -0.0556	0.05
1.0930 1.1305	-0.0356	0.05 0.05
1.0547	0.0200	0.05
1.0154	0.0951	0.05
0.9747	0.1695	0.05
0.9324 0.8884	0.2429 0.3154	0.05 0.05
0.8423	0.3865	0.05
0.7935	0.4558	0.05
0.7415	0.5227	0.05
0.6860 0.6266	0.5867 0.6472	0.05 0.05
0.5633	0.7035	0.05
0.4959	0.7550	0.05
0.4248	0.8010	0.05
0.3501	0.8410	0.05
0.2723 0.1920	0.8746 0.9018	0.05 0.05
0.1098	0.9222	0.05
0.0261	0.9358	0.05
-0.0583	0.9426	0.05
-0.1431	0.9427 0.9363	0.05 0.05
-0.2276 -0.3113	0.9233	0.05
-0.3938	0.9039	0.05
-0.4746	0.8782	0.05
-0.5531	0.8463	0.05
-0.6290 -0.7021	0.8087 0.7658	0.05 0.05
-0.7021	0.7180	0.05
-0.8390	0.6659	0.05
-0.9027	0.6101	0.05

X Inches	Y Inches	Z % Span
-0.9634	0.5509	0.05
-1.0211	0.4888	0.05
-1.0761	0.4243	0.05
-1.1285	0.3577	0.05
-1.1785	0.2893	0.05
-1.2260	0.2191	0.05
-1.2708	0.1471	0.05
-1.3123	0.0732	0.05
-1.3505	-0.0025	0.05
-1.3853	-0.0797	0.05
-1.4161	-0.1587	0.05
-1.4419	-0.2394	0.05
-1.4602	-0.3221 -0.4066	0.05 0.05
-1.4647 -1.4348	-0.4840	0.05
-1.4348	-0.4782	0.03
-1.2655	-0.4832	0.10
-1.1852	-0.4582	0.10
-1.1085	-0.4232	0.10
-1.0323	-0.3872	0.10
-0.9553	-0.3530	0.10
-0.8769	-0.3219	0.10
-0.7974	-0.2941	0.10
-0.7168	-0.2694	0.10
-0.6356	-0.2468	0.10
-0.5538	-0.2266	0.10
-0.4713	-0.2090	0.10
-0.3883	-0.1946	0.10
-0.3047	-0.1839	0.10
-0.2207	-0.1771	0.10
-0.1364	-0.1747	0.10
-0.0522	-0.1770	0.10
0.0318	-0.1842 -0.1966	0.10
0.1151 0.1976	-0.1988	$0.10 \\ 0.10$
0.1970	-0.2370	0.10
0.3583	-0.2647	0.10
	-0.2973	0.10
0.5117	-0.3344	0.10
0.5852	-0.3757	0.10
0.6563	-0.4209	0.10
0.7250	-0.4697	0.10
0.7913	-0.5217	0.10
0.8552	-0.5767	0.10
0.9167	-0.6343	0.10
0.9759	-0.6943	0.10

X	.Y	Z
Inches	Inches	% Span
1.0329 1.0877	-0.7564 -0.8205	0.10
1.1404	-0.8862	0.10
1.1912	-0.9535	0.10
1.2402	-1.0221	0.10
1.2880	-1.0915	0.10
1.3356	-1.1611	0.10
1.3903	-1.2240	0.10
1.4715	-1.2246	0.10
1.5193	-1.1588	0.10
1.5020	-1.0771	0.10
1.4727	-0.9981	0.10
1.4409	-0.9200	0.10
1.4085	-0.8422	0.10
1.3760	-0.7644	0.10
1.3434	-0.6867	0.10
1.3105	-0.6091	0.10
1.2775	-0.5315	0.10
1.2441	-0.4541	0.10
1.2103	-0.3769	0.10
1.1760	-0.2999	0.10
1.1412	-0.2232	0.10
1.1057	-0.1467	0.10
1.0695	-0.0706	0.10
1.0324	0.0051	0.10
0.9944	0.0803	0.10
0.9550	0.1549	0.10
0.9141	0.2286	0.10
0.8715	0.3013	0.10
0.8268	0.3728	0.10
0.7795	0.4425	0.10
0.7291	0.5101	0.10
0.6755	0.5751	0.10
0.6183	0.6370	0.10
0.5575	0.6954	0.10
0.4930	0.7496	0.10
0.4248	0.7991	0.10
0.3530	0.8432	0.10
0.2779	0.8815	0.10
0.2000	0.9137	0.10
0.1198	0.9394	0.10
0.0376	0.9580	0.10
-0.0459	0.9696	0.10
-0.1300 -0.2142	0.9741 0.9716	0.10
-0.2980	0.9622	0.10

Х	Y	Z
Inches	Inches	% Span
-0.3806	0.9458	0.10
-0.4617	0.9228	0.10
-0.5406	0.8932	0.10
-0.6170	0.8576 0.8163	0.10 0.10
-0.6904 -0.7607	0.7698	0.10
-0.8278	0.7698	0.10
-0.8915	0.6636	0.10
-0.9519	0.6049	0.10
-1.0092	0.5430	0.10
-1.0635	0.4786	0.10
-1.1150	0.4118	0.10
-1.1638	0.3431	0.10
-1.2101	0.2727	0.10
-1.2538	0.2006	0.10
-1.2940	0.1265	0.10
-1.3305	0.0506	0.10
-1.3636	-0.0269	0.10
-1.3928 -1.4171	-0.1060	0.10
-1.41/1 -1.4344	-0.1867 -0.2692	0.10 0.10
-1.4344	-0.3531	0.10
-1.4182	-0.4330	0.10
-1.2786	-0.4146	0.20
-1.1966	-0.4068	0.20
-1.1203	-0.3739	0.20
-1.0475	-0.3337	0.20
-0.9748	-0.2933	0.20
-0.9008	-0.2553	0.20
-0.8252	-0.2207	0.20
-0.7479	-0.1901	0.20
-0.6692	-0.1633	0.20
-0.5894 -0.5087	-0.1400	0.20 0.20
-0.5087 -0.4271	-0.1199 -0.1036	0.20
-0.4271	-0.0919	0.20
-0.2619	-0.0852	0.20
-0.1788	-0.0840	0.20
-0.0958	-0.0887	0.20
-0.0133	-0.0994	0.20
0.0682	-0.1161	0.20
0.1482	-0.1387	0.20
0.2264	-0.1668	0.20
0.3026	-0.2001	0.20
0.3766	-0.2380	0.20
0.4483	-0.2801	0.20

X	Y	Z		
Inches	Inches	% Span		110 30
0.5176	-0.3262	0.20		
0.5844	-0.3757	0.20		4.4.5
0.6488	-0.4282	0.20	٠.	
0.7110	-0.4834	0.20		
0.7710	-0.5411	0.20		4. 4
0.8288	-0.6008	0.20		
0.8847	-0.6624	0.20		$j = \frac{F_{ij}}{2} \frac{1}{2} 1$
0.9386	-0.7257	0.20		
0.9908	-0.7905	0.20		
1.0413	-0.8565	0.20		
1.0903	-0.9237	0.20		
1.1378	-0.9920	0.20		
1.1839	-1.0612	0.20		
1.2291	-1.1310	0.20		
1.2754	-1.2001	0.20		1.0
1.3309	-1.2610	0.20		
1.4112	-1.2619	0.20		
1.4594	-1.1977	0.20		
1.4454	-1.1164	0.20	-	Ŧ
1.4178	-1.0380	0.20		y
1.3872	-0.9606	0.20		
1.3558	-0.8836	0.20		
1.3241	-0.8067	0.20		r ·
1.2924	-0.7299	0.20		
1.2604	-0.6531	0.20		
1.2282	-0.5764	0.20		.*
1.1956	-0.4999	0.20	٠.	4
1.1626	-0.4235	0.20		
1.1292	-0.3474	0.20		
1.0953	-0.2715	0.20		to the second
1.0607	-0.1958	0.20		•
1.0255	-0.1205	0.20		
0.9895	-0.0455	0.20		
0.9526	0.0290	0.20		
0.9145	0.1030	0.20		
0.8752	0.1762	0.20		
0.8344	0.2487	0.20		
0.7918	0.3201	0.20		
0.7471	0.3902	0.20		
0.6998	0.4587	0.20		
0.6499	0.5251	0.20		
0.5970	0.5894	0.20		
0.5410	0.6508	0.20		
0.4815	0.7089	0.20		
0.4184	0.7630	0.20	•	
0.3517	0.8126	0.20	•	•

X	Y	Z	
Inches	Inches	% Span	
0.2815	0.8572	0.20	
0.2080	0.8962	0.20	
0.1315	0.9287	0.20	
0.0524	0.9543	0.20	
-0.0287	0.9724	0.20	
-0.1112	0.9830	0.20	
-0.1943	0.9861	0.20	
-0.2773	0.9817	0.20	
-0.3596	0.9700	0.20	
-0.4406	0.9513	0.20	
-0.5197	0.9257	0.20	
-0.5964	0.8937	0.20	
-0.6703	0.8556	0.20	
-0.7410	0.8118	0.20	,
-0.8082	0.7629	0.20	
-0.8719	0.7094	0.20	
-0.9319	0.6518	0.20	
-0.9883	0.5907	0.20	
-1.0414	0.5267	0.20	
-1.0912	0.4601	0.20	
-1.1380	0.3914	0.20	
-1.1822	0.3210	0.20	
-1.2235	0.2488	0.20	
-1.2609	0.1745	0.20	
-1.2944	0.0984	0.20	
-1.3242	0.0208	0.20	
-1.3498	-0.0584	0.20	
-1.3702	-0.1390	0.20	
-1.3830	-0.2211	0.20	
-1.3829	-0.3041	0.20	
-1.3527	-0.3803	0.20	
-1.2750	-0.3356	0.30	
-1.1951	-0.3497	0.30	
-1.1168	-0.3255	0.30	•
-1.0448	-0.2858	0.30	
-0.9748	-0.2427	0.30	
-0.9043	-0.2004	0.30	
-0.8322	-0.1608	0.30	
-0.7582	-0.1249	0.30	
-0.6823	-0.0932	0.30	
-0.6048	-0.0657	0.30	
-0.5260	-0.0423	0.30	
-0.4459	-0.0233	0.30	
-0.3648	-0.0097	0.30	
-0.2830	-0.002.0	0.30	
-0.2007	-0.0011	0.30	

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1.2784 -0.8591 0.30 1.2472 -0.7830 0.30 1.2157 -0.7070 0.30 1.1840 -0.6311 0.30 1.1518 -0.5554 0.30 1.1193 -0.4798 0.30 1.0864 -0.4044 0.30 1.0530 -0.3293 0.30 1.0190 -0.2544 0.30 0.9844 -0.1798 0.30 0.9491 -0.1055 0.30 0.9130 -0.0316 0.30					
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1.2157 -0.7070 0.30 1.1840 -0.6311 0.30 1.1518 -0.5554 0.30 1.1193 -0.4798 0.30 1.0864 -0.4044 0.30 1.0530 -0.3293 0.30 1.0190 -0.2544 0.30 0.9844 -0.1798 0.30 0.9491 -0.1055 0.30 0.9130 -0.0316 0.30					
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0.9491 -0.1055 0.30 0.9130 -0.0316 0.30					
0.9130 -0.0316 0.30					
·		,			
0.8759 0.0419 0.30	0.8759	0.0419	0.30		
0.7986 0.1871 0.30					
0.8378				*	A A

	37	V	Z		
	" X	Y	% Span		
e 1 42	Inches	Inches	% Span		
:	0.7580	0.2586	0.30		
	0.7157	0.3291	0.30		
•	0.6715	0.3985	0.30		
	0.6251	0.4664	0.30		
	0.5762	0.5325	0.30		
		0.5965	0.30		
	0.4696	0.6578	0.30		
	0.4113	0.7157	0.30		4
	0.3493	0.7698	0.30		
	0.2838	0.7030	0.30		* *
	0.2147	0.8641	0.30		
		0.8041	0.30	;	•
	0.1422		0.30		
``.	0.0664	0.9347			
	-0.0121	0.9592	0.30	•	
•	-0.0925	0.9762	0.30		
	-0.1742	0.9854	0.30		
	-0.2564	0.9868	0.30		*, *,
	-0.3384	0.9803	0.30		
	-0.4194	0.9663	0.30		
	-0.4988	0.9448	0.30		
•	-0.5759	0.9162	0.30	•	
	-0.6501	0.8808	0.30		
	-0.7209	0.8390	0.30		
	-0.7880	0.7915	0.30		
•	-0.8512	0.7389	0.30		
- *	-0.9105	0.6818	0.30		•
	-0.9658	0.6210	0.30	•	• •
e e	-1.0175	0.5570	0.30	-	
1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	-1.0657	0.4903	0.30		1. A. J. J. W.
i, taka ta	-1.1107	0.4215	0.30		Control of the second
٠,	-1.1531	0.3511	0.30		
	-1.1922	0.2787	0.30		
	-1.2272	0.2043	0.30	•	
	-1.2583	0.1282	0.30	•	r.
2.1	-1.2855	0.0505	0.30	•	
	-1.3081	-0.0285	0.30		
1	-1.3249	-0.1090	0.30		
	-1.3326	-0.1909	0.30		
	-1.3236	-0.2723	0.30		
- -	-1.2050	-0.2886	0.40		
	-1.1248	-0.2873	0.40		
	-1.0503	-0.2554	0.40		
	-0.9807	-0.2135	0.40		
	-0.9123	-0.1698	0.40		* * * * * * * * * * * * * * * * * * * *
	-0.8431	-0.1272	0.40		
	-0.7723	-0.1272	0.40		
F	-0.1123	-0.00/4	0.40		*

X Inches	Y Inches	Z % Span
-0.6996	-0.0513	0.40
-0.6250	-0.0192	0.40
-0.5486	0.0085	0.40
-0.4707	0.0314	
-0.3913	0.0484	0.40
-0.3108	0.0585	0.40
-0.2296	0.0608	
-0.1486	0.0548	0.40
-0.0688	0.0403	0.40
0.0093	0.0178	0.40
0.0848	-0.0119	0.40
0.1575	-0.0481	0.40
0.2271	-0.0899	0.40
0.2937	-0.1364	0.40
0.3574	-0.1867 -0.2403	$0.40 \\ 0.40$
0.4185 0.4770	-0.2966	0.40
0.4770	-0.3552	0.40
0.5332	-0.4158	0.40
0.6396		0.40
0.6902	-0.5415	0.40
0.7393	-0.6062	0.40
0.7870	-0.6719	0.40
0.8334	-0.7386	0.40
0.8788	-0.8060	0.40
0.9231	-0.8740	0.40
0.9665	-0.9427	0.40
1.0091	-1.0118	0.40
1.0510	-1.0814	0.40
1.0921	-1.1514	0.40
1.1335	-1.2213	0.40
1.1765	-1.2902	0.40
1.2295	-1.3506	0.40
1.3079	-1.3522	0.40
1.3566	-1.2906	0.40
1.3452	-1.2109	0.40
1.3202	-1.1336	0.40
1.2913	-1.0577	0.40
1.2613	-0.9822	0.40
1.2310	-0.9069	0.40
1.2006 1.1699	-0.8316 -0.7564	0.40 0.40
1.1389	-0.6813	0.40
1.1389	-0.6064	0.40
1.0758	-0.5316	0.40
1.0437	-0.4570	0.40
T.0401	0.4010	0.40

Χ	. У	Z	÷.
Inches	Inches	% Span	
1 0111	0 2026	0.40	
1.0111	-0.3826	0.40	
0.9781	-0.3084	0.40	
0.9444	-0.2345	0.40	
0.9101	-0.1608	0.40	
0.8752	-0.0875	0.40	
0.8394	-0.0146	0.40	
0.8028	0.0579	0.40	
0.7653	0.1299	0.40	
0.7266	0.2014	0.40	
0.6866	0.2720	0.40	
0.6450	0.3418	0.40	•
0.6016	0.4105	0.40	
0.5562	0.4778	0.40	
0.5084	0.5434	0.40	
0.4576	0.6068	0.40	
0.4037	0.6676	0.40	
0.3465	0.7252	0.40	
0.2858	0.7792	0.40	
0.2216	0.8289	0.40	
0.1537	0.8735	0.40	, '
0.0822	0.9119	0.40	
0.0075	0.9436	0.40	
-0.0700	0.9680	0.40	
-0.1495	0.9844	0.40	
-0.2303	0.9924	0.40	· ·
-0.3115	0.9918	0.40	
-0.3921	0.9825	0.40 0.40	
-0.4713	0.9645 0.9382	0.40	
-0.5481 -0.6217	0.9362	0.40	The second secon
	0.8629	0.40	
-0.6917 -0.7577	0.8156	0.40	
-0.7377	0.7629	0.40	\mathcal{L}_{i}
-0.8193	0.7057	0.40	
-0.9309	0.6448	0.40	
-0.9809	0.5809	0.40	
-1.0276	0.5144	0.40	
-1.0276	0.4459	0.40	
-1.1124	0.3759	0.40	
-1.1124 -1.1503	0.3041	0.40	
-1.1303 -1.1845	0.2304	0.40	
-1.1645 -1.2149	0.2504	0.40	
-1.2149 -1.2413	0.1331	0.40	
-1.2413 -1.2629	0.0000	0.40	
-1.2029	-0.0797	0.40	•
	-0.1607	0.40	
-1.2830	-0.1007	0.40	

	X	Y	Z); }
	Inches I	nches	% Span	•	and the second
	-1.2663 -0	0.2396	0.40		
	-1.2115 -0	0.2017	0.50	, 1 -	· · · · · · · · · · · · · · · · · · ·
	-1.1425 -0	0.2377	0.50		
	-1.0641 -0	0.2257	0.50		
*	-0.9921 - 0	0.1906	0.50		. (* 1)
		0.1487	0.50		e i ed e
. •		0.1058	0.50		
1.		0.0642	0.50		
		0.0254	0.50		
		.0098	0.50		a transfer of
		.0409	0.50		
		.0674	0.50		A Comment
		.0880	0.50		And the second
		.1013	0.50		
٠.		.1061	0.50	i	
		.1014	0.50		
		.0871	0.50		
3.		.0636	0.50		
. •,		.0321	0.50		
		0.0063	0.50		
		0.0505	0.50		2
		0.0992	0.50		
		0.1518	0.50		
		0.2074	0.50		
		0.2654	0.50		
		0.3255	0.50		. A
		0.3873	0.50		
		0.4505	0.50		Section 1985
		0.5149	0.50		
		0.5803	0.50	•	
- ; -		0.6465	0.50		
* 1		0.7135	0.50		
		7811	0.50	:	1. 19.
		0.8492	0.50		
:		0.9178	0.50	1 1	
		9868	0.50		
		1.0562	0.50	v.	
		l.1258	0.50		
		1.1958	0.50		
		1.2655	0.50		
		1.3342	0.50		
		1.3939	0.50		
		1.3956	0.50		
		1.3354	0.50		* * * * * * * * * * * * * * * * * * *
		1.2566	0.50	·	
4.		L.1802	0.50		**************************************
	~ · - · · · - ·				* *

	; X	· Y	Z	•	
and the second	Inches	Inches	% Span		er in the state of the
	1.2424	-1.1050	0.50		1. 1.31.4.4.
	1.2133	-1.0304	0.50	et .	
* - *	1.1840	-0.9558	0.50	25	
	1.1546	-0.8813	0.50		
1.5	1.1249	-0.8069	0.50	• .	
* 2 * 2 * 2 * 2 * 2 * 2 * 2 * 2 * 2 * 2	1.0950	-0.7325	0.50		
	1.0647	-0.6583	0.50	•	S. J. J. J.
	1.0341	-0.5843	0.50	10.00	
10000	1.0032	-0.5104	0.50		
$r^* = r^*$	0.9718	-0.4366	0.50	*,	
	0.9400	-0.3631	0.50		
· · · · · · · · · · · · · · · · · · ·	0.9077	-0.2898	0.50		•
3 - 5 - 5 - 5 - 5	0.8748	-0.2167	0.50		Same Carter
	0.8413	-0.1439	0.50		(Forest Control
F. 14	0.8072	-0.0714	0.50		4 - 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
•	0.7723	0.0007	0.50	* *	
	0.7365	0.0724	0.50	1	*** *** **** **** **** **** **** **** ****
* * *	0.6998	0.1436	0.50		
and the second	0.6619	0.2142	0.50		- 1
· · · · · · · · · · · · · · · · · · ·	0.6227	0.2841	0.50		
Maria Maria	0.5821	0.3531	0.50		
	0.5397	0.4212	0.50		
	0.4954	0.4879	0.50		
•	0.4485	0.5529	0.50	,	. 5.
Ÿ	0.3989	0.6158	0.50		
e de la serie de la companya della companya della companya de la companya della c	0.3464	0.6763	0.50	•	
	0.2908	0.7340	0.50		
.,	0.2318	0.7882	0.50		
· · · · · · · · · · · · · · · · · · ·	0.1692	0.8382	0.50		
	0.1028	0.8830	0.50	*	A
	0.0328	0.9218	0.50		
<i>a</i> . •	-0.0407	0.9537	0.50	4 - 4	
	-0.1171	0.9777	0.50	•	
	-0.1958	0.9928	0.50		
	-0.2757	0.9985	0.50		4
	-0.3556	0.9943	0.50		* * * * *
•	-0.4344	0.9801	0.50		
* · · · · · · · · · · · · · · · · · · ·	-0.5109	0.9564	0.50		
	-0.5842	0.9240	0.50		the things
•	-0.6535	0.8839	0.50		
	-0.7186	0.8372	0.50		H14.7.27.1
	-0.7794	0.7850	0.50		
·	-0.8360	0.7284	0.50		
• .	-0.8887		0.50		*
•	-0.9378	0.6047	0.50		33° 2
•	-0.9836	0.5390	0.50	•	建设建设

X	Y	Z		· 3
Inches	Inches	% Span		A. A. S. A.
-1.0265	0.4713	0.50		
-1.0670	0.4022	0.50		
-1.1046	0.3314	0.50		
-1.1389	0.2590	0.50		San San San
-1.1695	0.1850	0.50		and the second
-1.1961	0.1094	0.50	3	1
-1.2178	0.0323	0.50	2 -	+ <i>4</i>
- 1.2325	-0.0464	0.50		, %.
-1.2355	-0.1264	0.50		
-1.1511	-0.1583	0.60	:	100
-1.0760	-0.1775	0.60	•	
-1.0003	-0.1557	0.60		ta esta esta esta esta esta esta esta es
-0.9305	-0.1185	0.60		
-0.8631	-0.0771	0.60	**************************************	
-0.7956	-0.0358	0.60	1.14	and the second
-0.7269	0.0035	0.60	•	
-0.6565	0.0395	0.60	7	; ;
-0.5841	0.0715	0.60	4 * · · · · · · ·	
-0.5099	0.0990	0.60	1 - 1	
-0.4339	0.1208	0.60		and the state of t
-0.3562	0.1355	0.60	**	
-0.2773	0.1413	0.60		
-0.1983	0.1372	0.60		. 13 m n n
-0.1206	0.1228	0.60	1	
-0.0453	0.0985	0.60		
0.0266	0.0655	0.60	*	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.0947	0.0254	0.60		
0.1591	-0.0206	0.60		
0.2199	-0.0712	0.60	•	
0.2775	-0.1255	0.60		
0.3321	-0.1827	0.60		
0.3843	-0.2422	0.60		
0.4343	-0.3036	0.60	•	
0.4823	-0.3665	0.60	***	
0.5285	-0.4307	0.60		
0.5733	-0.4959	0.60		
0.6168	-0.5620	0.60		
0.6591	-0.6289	0.60		
0.7004	-0.6964	0.60		
0.7408	-0.7644	0.60		
0.7804	-0.8329	0.60	,	
0.8193	-0.9018	0.60		
0.8577	-0.9710	0.60		
0.8956	-1.0405	0.60		
0.9330	-1.1102	0.60		
0.9701	-1.1801	0.60	•	

2 X	Y	Z		;	* *** * **
Inches	Inches	% Span			2000
1.0069	-1.2502	0.60			
1.0442	-1.3200	0.60	;		100
1.0832	-1.3888	0.60			
1.1330	-1.4488	0.60	•		
1.2095	-1.4510	0.60			2 4 4 5
1.2585	-1.3921	0.60			
1.2494	-1.3143	0.60			
1.2258	-1.2388	0.60			
1.1991	-1.1643	0.60	ŧ	. *	
1.1711	-1.0903	0.60		0	
1.1430	-1.0163	0.60			
1.1146	-0.9424	0.60		•	And the second
1.0861	-0.8686	0.60		*	5. A
1.0573	-0.7949	0.60	•		1.0
1.0283	-0.7213	0.60			er vijervije in
0.9990	-0.6478	0.60		•	4.7
0.9693	-0.5744	0.60			A STATE
0.9393	-0.5012	0.60			
0.9089	-0.4282	0.60			
0.8780	-0.3553	0.60	,		
0.8467	-0.2826	0.60			
0.8147	-0.2102	0.60			100
0.7822	-0.1381	0.60		*	1
0.7491	-0.0663	0.60		,	4.1
0.7152	0.0053	0.60			: .
0.6804	0.0764	0.60		*	1 3
0.6447	0.1470	0.60			$\gamma_{i} = \begin{pmatrix} \gamma_{i} & \gamma_{i} & \gamma_{i} \\ 1 & 2 \end{pmatrix} = \gamma_{i}$
0.6078	0.2170	0.60	·		x = x + 1 + 1 - 3
0.5698	0.2864	0.60			$Q = \operatorname{Wind}(1)$
0.5304	0.3550	0.60			
0.4892	0.4226	0.60			Section 18
0.4461	0.4889	0.60	\$ 1		
0.4006	0.5536	0.60			1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
0.3525	0.6165	0.60	-	÷	$\mathcal{M}_{s}((p,p))^{1/p}$
0.3017	0.6771	0.60			$(\alpha_{i+1},\dots,\alpha_{i-1})^{-1}$
0.2478	0.7351	0.60	.*		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.1904	0.7895	0.60			19 1 1 1 A
0.1292	0.8396	0.60			
0.0640	0.8845	0.60	4		2 1 1 1 1 1
-0.0050	0.9231	0.60			· 1 2 1 1 1 1 1
-0.0777	0.9541	0.60			The State of
-0.1536	0.9766	0.60		•	ere e
-0.2316	0.9893	0.60	•		
-0.3107	0.9917	0.60			
-0.3893	0.9834	0.60			
-0.4662	0.9649	0.60			100

X	У , У	Z		
Inches	Inches	% Span	1 8	18 to
-0.5401	0.9368	0.60		
-0.6103	0.9003	0.60		5
-0.6762	0.8566	0.60	*	
-0.7377	0.8069	0.60		
-0.7948	0.7522	0.60		
-0.8479	0.6934	0.60		100
-0.8971	0.6315	0.60		(1) H = 1 +
-0.9429	0.5670	0.60		me in the
-0.9857	0.5004	0.60		200
-1.0257	0.4322	0.60		
-1.0630	0.3624	0.60	*	
-1.0971	0.2910	0.60		1
-1.1275	0.2179	0.60		£_ 2
-1.1537	0.1433	0.60		
-1.1748	0.0670	0.60	•	← x x ⁻¹
-1.1880	-0.0109	0.60		Company of the
-1.1870	-0.0898	0.60		24 - 4 - 3 - 3 - 3
-1.0894	-0.1069	0.70	•	· vi
-1.0127	-0.1117	0.70		j
-0.9399	-0.0839	0.70		•
-0.8715	-0.0461	0.70		
-0.8044	-0.0061	0.70		
-0.7366	0.0327	0.70		
-0.6672	0.0686	0.70		•
-0.5958	0.1003	0.70		
-0.5225	0.1273	0.70		
-0.4473	0.1486	0.70		
-0.3705	0.1628	0.70		the grade of the first
-0.2926	0.1682	0.70		
-0.2147	0.1635	0.70		
-0.1382	0.1481	0.70		
-0.0644	0.1226	0.70	1	
0.0058	0.0882	0.70 0.70	-	
0.0718	0.0466 -0.0008	0.70	•	
0.1339 0.1923	-0.0527	0.70		
0.1923	-0.1082	0.70		
0.2994	-0.1665	0.70		
0.3489	-0.2270	0.70		
0.3961	-0.2892	0.70		
0.4415	-0.3528	0.70		
0.4851	-0.4176	0.70		•
0.5273	-0.4834	0.70		•
0.5681	-0.5500	0.70		
0.6079	-0.6172	0.70		· · · · · · · · · · · · · · · · · · ·
0.6467	-0.6851	0.70		
0.0107	2.0001	_ , , ,		

	17	-		
X	Y	Z ° C====		+ A
Inches	Inches	% Span	Att Action	A CONTRACTOR
0.6846	-0.7534	0.70	*	
0.7218	-0.8221	0.70		
0.7584	-0.8911	0.70		4, 23
0.7945	-0.9605	0.70		
0.8301	-1.0300	0.70		
0.8654	-1.0997	0.70		
0.8654	-1.1696	0.70		
0.9003		0.70		· · · · · · · · ·
	-1.2396		*	
0.9698	-1.3096	0.70	•	
1.0050	-1.3794	0.70		
1.0415	-1.4484	0.70		
1.0900	-1.5081	0.70	,	
1.1654	-1.5109	0.70		
1.2142	-1.4531	0.70		
1.2060	-1.3763	0.70		, * · · · · · · · · · · · · · · · · · ·
1.1831	-1.3016	0.70		31.11
1.1573	-1.2278	0.70		
1.1305	-1.1544	0.70		
1.1036	-1.0811	0.70		• • •
1.0765	-1.0078	0.70		
1.0492	-0.9346	0.70		
1.0217	-0.8615	0.70	-	2
0.9939	-0.7884	0.70		•
0.9659	-0.7155	0.70		
0.9377	-0.6426	0.70		
0.9090	-0.5699	0.70		3 2/2
0.8801	-0.4974	0.70		,
0.8507	-0.4250	0.70		
0.8209	-0.3527	0.70		1.00
0.7906	-0.2807	0.70		and Theorem
0.7598	-0.2089	0.70		
0.7284	-0.1373	0.70°		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.6964	-0.0661	0.70	•	+ 1,3-1
0.6636	0.0049	0.70		. 1
0.6300	0.0754	0.70		
0.5955	0.1455	0.70		
0.5600	0.2151	0.70		
0.5233	0.2841	0.70	***;	1.50
0.4852	0.3523	0.70		
0.4455	0.4196	0.70		
0.4038	0.4857	0.70		100
0.3599	0.5503	0.70		
0.3137	0.6133	0.70		
0.2646	0.6741	0.70		
0.2122	0.7321	0.70	•	•
0.1562	0.7865	0.70		
0.1002	0.7005	0.70		

	X	Y	Z		. 4,
1.7	Inches	Inches	% Span		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	0.0962	0.8366	0.70		San Argon
À	0.0321	0.8812	0.70	2 N 2	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	-0.0362	0.9191	0.70	5	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
	-0.1083	0.9490	0.70		1 J. J. 1885
ALC: 1	-0.1836	0.9696	0.70	,	
	-0.2610	0.9799	0.70		15 大学 150 (1887) 12 (1887)
	-0.3391	0.9793	0.70	. F	A STATE OF THE STATE OF
	-0.4163	0.9679	0.70	8.	
	-0.4913	0.9462	0.70		₹ · · · · · · · · · · · · · · · · · · ·
2	-0.5630	0.9152	0.70		Company Carlotter
£ + .	-0.6306	0.8760	0.70	44.1	St. B. Santa
: .	-0.6936	0.8300	0.70		
	-0.7521	0.7782	0.70		the state of the s
	-0.8062	0.7218	0.70		
	-0.8562	0.6618	0.70		the second of the
, ,	-0.9024	0.5988	0.70		and the second second second second
: " · :	-0.9452	0.5334	0.70		The state of the s
-	-0.9849	0.4661	0.70		
	-1.0219	0.3973	0.70		Harry Company
	-1.0558	0.3269	0.70	•	
• * • •	-1.0859	0.2548	0.70		
-	-1.1117	0.1811	0.70		
	-1.1320	0.1057	0.70	-	, , ,
ř .	-1.1435	0.0284	0.70		
7	-1.1377	-0.0491	0.70		
	-1.0375	-0.0483	0.80		
	-0.9616	-0.0453	0.80		
*	-0.8907	-0.0156	0.80		and Market Speed
	-0.8232	0.0215	0.80		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	-0.7561	0.0594	0.80	•	
	-0.6878	0.0950	0.80 0.80		
	-0.6176	0.1266 0.1531	0.80		
	-0.5452	0.1331	0.80		1000年,1000年, 1000年,1000年末日
,	-0.4710 -0.3951	0.1755	0.80		
- '	-0.3183	0.1906	0.80		
	-0.2416	0.1300	0.80		and the second seco
	-0.1666	0.1671	0.80		and the second second
	-0.0946	0.1398	0.80		
	-0.0265	0.1038	0.80	•	
•	0.0372	0.0606	0.80		
	0.0372	0.0119	0.80		10 10 10 10 10 10 10 10 10 10 10 10 10 1
	0.1527	-0.0411	0.80		en e
	0.2053	-0.0411	0.80		
,	0.2550	-0.0574	0.80		
	0.3021	-0.1303	0.80	•	
	0.3021	27		\$ [*]	
		<i>L 1</i>			

4	X	Y	Z		•
	Inches	Inches	% Span		* * * · · · · · · · · · · · · · · · · ·
			_		
1. 1. 1	0.3471	-0.2797	0.80		
	0.3903	-0.3435	0.80		
	0.4318	-0.4083	0.80		
	0.4719	-0.4741	0.80	*	And the state of t
and the second second	0.5108	-0.5406	0.80	# **	
2-1-2	0.5487	-0.6076	0.80		4 - 4 - 7
	0.5856	-0.6752	0.80		
The second second	0.6218	-0.7432	0.80	18.	to Desire the
* * *	0.6573	-0.8116	0.80		
•	0.6922	-0.8803	0.80		
* * * * * *	0.7266	-0.9492	0.80		
er e	0.7606	-1.0183	0.80		*
# * · · · · · · · · · · · · · · · · · ·	0.7944	-1.0875	0.80	1.0	the state of the s
the decision of	0.8279	-1.1569	0.80		
1	0.8612	-1.2263	0.80		
4 - 1 - 1 - 1 - 1	0.8944	-1.2958	0.80	,	1.00
, , •	0.9277	-1. 3653	0.80		
	0.9615	-1.4345	0.80	V 1	$\mathcal{F} = \{ \frac{1}{2}, \dots, \frac{1}{2}, \dots, \frac{1}{2} \}$
A Comment of the Comment	0.9966	-1.5030	0.80		the state of the s
And the second	1.0441	-1.5620	0.80		
	1.1186	-1.5651	0.80		
	1.1664	-1.5079	0.80		
	1.1602	-1.4 322	0.80		
· · · · · · ·	1.1374	-1.3586	0.80		
	1.1126	-1.2857	0.80		the second second
	1.0870	-1.2131	0.80	•	· · · · · · · · · · · · · · · · · · ·
and the second	1.0612	-1.1405	0.80		
	1.0354	-1.0679	0.80	1000	the contract of
	1.0093	-0.9954	0.80		
1	0.9831	-0.9230	0.80		
* * * * * * * * * * * * * * * * * * *	0.9567	-0.8507	0.80		
	0.9301	-0.7784	0.80	1. 1. 1. 1. 1. 1. 1.	And Anti-
	0.9032	-0.7062	0.80		
	0.8760	-0.6341	0.80	• •	
	0:8485	-0.5622	0.80		1000
	0.8206	-0.4904	0.80		
	0.7924	-0.4187	0.80	÷ .	
· '. '. '.	0.7638	-0.3472	0.80	4 1	and the second second
	0.7346	-0.2759	0.80		
	0.7051	-0.2048	0.80		the state of the s
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.6749	-0.1339	0.80		
. 7.	0.6442	-0.0633	0.80		
	0.6127	0.0070	0.80		
	0.5805	0.0770	0.80		
	0.5474	0.1466	0.80		
	0.5133	0.2157	0.80		
•		28			
		_ •			

X	Y	Z ·		No.
Inches	Inches	% Span		Emplication (
0.4782	0.2842	0.80		0.45
0.4416	0.3520	0.80		
0.4035	0.4189	0.80		
0.3636	0.4848	0.80	the second	
0.3217	0.5494	0.80	•	
0.2773	0.6124	0.80	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	
0.2301	0.6732	0.80		
0.1796	0.7313	0.80.		10 mg/mg/mg/mg/mg/mg/mg/mg/mg/mg/mg/mg/mg/m
0.1252	0.7859	0.80		4.5
0.0668	0.8361	0.80		
0.0040	0.8806	0.80	,	1 3,600
-0.0632	0.9182	0.80	•	1.4
-0.1344	0.9474	0.80		1 m 2 1
-0.2089	0.9667	0.80		(): :
-0.2854	0.9751	0.80		1.8
-0.3623	0.9723	0.80		
0.4380	0.9583	0.80		
-0.5110	0.9339	0.80		
-0.5803	0.9004	0.80	•	, - , - , -
-0.6452	0.8589	0.80		
-0.7053	0.8109	0.80		100
-0.7608	0.7575	0.80		* * * * * * * * * * * * * * * * * * * *
-0.8117	0.6997	0.80		
-0.8586	0.6386	0.80	•	
-0.9016	0.5747	0.80		No. of the second
-0.9413	0.5087	0.80		
-0.9782	0.4411	0.80		en e
-1.0120	0.3719	0.80		
-1.0421	0.3010	0.80		
-1.0681	0.2285	0.80		
-1.0883	0.1542	0.80		The Desire
-1.0995	0.0781	0.80		
-1.0914 -0.9953	0.0020 0.0156	0.80		
-0.9206	0.0130	0.90		
-0.8509	0.0513	0.90		
-0.7839	0.0869	0.90	-	
-0.7167	0.1220	0.90	% 	
-0.6478	0.1538	0.90		en e
-0.5768	0.1803	0.90		and the first
-0.5036	0.2002	0.90		
-0.4287	0.2125	0.90	4 6 2	
-0.3530	0.2153	0.90		
-0.2777	0.2067	0.90		
-0.2046	0.1867	0.90		1.5
-0.1351	0.1563	0.90		
	0.0	•		

	₹ X	y Y	Z		ý
•	Inches	Inches	% Span	••	Carrier A
	-0.0700	0.1174	0.90	e e e e e e e e e e e e e e e e e e e	
	0.0093	0.0719	0.90		49 1383
	0.0473	0.0214	0.90	•	The second secon
i i i	0.1003	-0.0328	0.90	, ÷	A Comment of the second
	0.1503	-0.0899	0.90		S. 150
•	0.1976	-0.1492	0.90		in the state of th
• • •	0.2426	-0.2103	0.90	+ *	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
9	0.2856	-0.2728	0.90		
1. 1. 1. 1.	0.3270	-0.3364	0.90		
	0.3670	-0.4009	0.90	to the transfer of	1. 14. 14. 14. 14. 14. 14. 14. 14. 14. 1
and the first	0.4057	-0.4661	0.90		$\chi_{i_1}^{\bullet} = \hat{\chi}_{i_2}^{\bullet}$
7 76.	0.4433	-0.5320	0.90		
1 . All 1	0.4799	-0.5985	0.90	* · · · · · · · · · · · · · · · · · · ·	
	0.5157	-0.6654	0.90		
	0.5509	-0.7326	0.90	$(x,y) = (x,y) \cdot \frac{\partial y}{\partial x} = 0$	
	0.5854	-0.8002	0.90	· ·	
* * * * * * * * * * * * * * * * * * *	0.6194	-0.8680	0.90		
	0.6529	-0.9361	0.90		
et de la company	0.6861	-1.0043	0.90		
•	0.7190	-1.0727	0.90		
	0.7517	-1.1411	0.90		the state of
	0.7842	-1.2097	0.90		A section
	0.8166	-1.2783	0.90		And the second
10 P. A.	0.8490	-1.3469	0.90		
e e e e e e e e e e e e e e e e e e e	0.8813	-1.4155	0.90		
	0.9141	-1.4839	0.90		
	0.9482	-1.5517	0.90		
	0.9953	-1.6095	0.90		
	1.0688	-1.6126	0.90		
	1.1186	-1.5584	0.90		
	1.1127	-1.4840	0.90		
	1.0901	-1.4116	0.90		
	1.0661	-1.3396	0.90		and Arthurst Control
	1.0417	-1.2677	0.90		
	1.0171	-1.1960	0.90		
	0.9924	-1.1242	0.90 0.90		
	0.9677	-1.0525		*	
en e	0.9427	-0.9808	0.90		A Maria
	0.9176	-0.9092	0.90	· .	the Alberta
	0.8923	-0.8377	0.90	•	
	0.8668	-0.7662	0.90		
	0.8411	-0.6949	0.90		• 1
	0.8151	-0.6236	0.90	± - 1	
	0.7888	-0.5524	0.90		100 (m)
	0.7621	-0.4814	0.90	• •	•
	0.7351	-0.4105	0.90		į.
		30			

Х ,	Y	\mathbf{Z}_{\cdot}		
Inches	Inches	% Span		in the second
0.7077	-0.3397	0.90		1
0.6799	-0.2692	0.90		the state of
0.6516	-0.1988	0.90		1.0%
.0.6228	-0.1286	0.90	***	
0.5934	-0.0586	0.90		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0.5633	0.0110	0.90		1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
0.5326	0.0804	0.90	•	,44 <u>(</u>
0.5010	0.1494	0.90		
0.4685	0.2179	0.90	*	
0.4348	0.2859	0.90		$x = x^{\alpha} = x^{\alpha} = -e^{\alpha}$
0.3999	0.3533	0.90	** .	•
0.3636	0.4199	0.90		
0.3256	0.4856	0.90		
0.2857	0.5501	0.90		
0.2434	0.6131	0.90		
0.1983	0.6741	. 0.90		· - γ · ·
0.1499	0.7325	0.90		· * *
0.0977	0.7875	0.90		
0.0413	0.8382	0.90	•	43
-0.0197	0.8834	0.90		
-0.0854	0.9213	0.90		
-0.1554	0.9504	0.90	•	•
-0.2288	0.9692	0.90		***
-0.3042	0.9764	0.90		;
-0.3799	0.9718	0.90		
-0.4540	0.9557	0.90		and the second of the second o
-0.5250	0.9292	0.90		
-0.5920	0.8937	0.90		
-0.6543	0.8504	0.90		
-0.7116	0.8008	0.90		
-0.7640	0.7460	0.90		
-0.8119	0.6871	0.90		
-0.8556	0.6251 0.5606	0.90 0.90		
-0.8956		0.90		
-0.9325	0.4944			•
-0.9664	0.4265	0.90 0.90		en e
-0.9969	0.3570			
-1.0233	0.2859	0.90		
-1.0444	0.2130	0.90		
-1.0566	0.1382	0.90 0.90	•	
-1.0498	0.0632 0.0490	0.90		
-0.9757			•	
-0.9016	0.0557	0.95 0.95		
-0.8324 -0.7656	0.0853	0.95		
	0.1200	0.95		
-0.6982	0.1537	0.95	•	•

	· X	Y	Z					4,
	Inches	Inches	% Span					A Description
	-0.6290	0.1833	0.95					ž .
	-0.5575 -	0.2069	0.95					
	-0.4839	0.2230	0.95					4.65.4
	-0.4091	0.2308	0.95					
	-0.3339	0.2280	0.95					1 1337
	-0.2602	0.2127	0.95					
<i>.</i> .	-0.1899	0.1858	0.95					
	-0.1242	0.1490	0.95					
	-0.0634	0.1047	0.95					
	-0.0068	0.0550	0.95					
	0.0460	0.0013	0.95					
	0.0958	-0.0552	0.95					
	0.1428	-0.1140	0.95		•			
	0.1877	-0.1745	0.95					
	0.2306	-0.2364	0.95					•
	0.2719	-0.2995	0.95					
	0.3117	-0.3634	0.95		S 1.			
	0.3503	-0.4281	0.95					
	0.3879 .	-0.4934	0.95			,		• •
	0.4245	-0.5592	0.95					
	0.4603	-0.6255	0.95				-	
	0.4954	-0.6921	0.95					
	0.5298	-0.7591	0.95					•
	0.5638	-0.8263	0.95					ϵ_{i}
	0.5973	-0.8938	0.95					
	0.6304	-0.9615	0.95		*		1	
4	0.6633	-1.0293	0.95		,			1 1 1
	0.6958	-1.0972	0.95		1 200			$\mathcal{T} = m_{k+1} - \epsilon_k = -1$
	0.7282	-1.1652	0.95					7 - 1 - 11 3
	0.7604	-1.2333	0.95					
	0.7925	-1.3014	0.95					
	0.8246	-1.3696	0.95		-			An experience of the second se
	0.8567	-1.4377	0.95					- N
•	0.8891 -	-1.5057	0.95					
-	0.9227	-1.5731	0.95	٠.				14
	0.9698	-1.6302	0.95					
	1.0428	-1.6333	0.95		٠.		-	
	1.0942	-1.5817	0.95					* * * * * * * * * * * * * * * * * * *
	1.0881	-1.5078	0.95		•			3 - +
	1.0656	-1.4359	0.95					*
	1.0421	-1.3643	0.95					1
	1.0182	-1.2929	0.95					*
	0.9942	-1.2215	0.95		-			1
	0.9701	-1.1501	0.95		-			the property of
	0.9460	-1.0788	0.95					
	0.9217	-1.0075	0.95					
		0.0						

1 38

			• •			
	X	· Y	\mathbf{z}			
•	Inches	Inches	% Span	•	٠ .	San
	0 0072	0 0363	0.05			
	0.8972	-0.9362	0.95	•		** ** ** ** ** ** ** ** ** ** ** ** **
	0.8726	-0.8650	0.95	·	•	
	0.8477	-0.7939	0.95			
•	0.8227	-0.7229	0.95	* * * * * * * * * * * * * * * * * * * *		
	0.7974	-0.6519	0.95			
• .	0.7718	-0.5811	0.95			$\mathcal{F}_{i}^{n} = \mathcal{F}_{i}^{n} = 0$
	0.7459	-0.5103	0.95			18 0000
	0.7197	-0.4397	0.95			War Carlo
	0.6932	-0.3692	0.95	· ·		$(-1)^{n} = \delta_{n} = (-1)^{n}$
•	0.6662	-0.2989	0.95	•		St. 5 %.
	0.6388	-0.2287	0.95			eri jedija
	0.6110	-0.1587	0.95			1.0
4 · *	0.5826	-0.0890	0.95			Constant
-	0.5535	-0.0194	0.95	4 7 7 1		Special Control
	0.5238	0.0498	0.95			રા કરવામાં
	0.4934	0.1187	0.95			
	0.4621	0.1872	0.95			j reti
* *	0.4298	0.2552	0.95			The Control of the Control
	0.3963	0.3227	0.95			
	0.3616	0.3896	0.95			
	0.3254	0.4556	0.95			
	0.2875	0.5207	0.95			
÷	0.2476	0.5846	0.95			
:	0.2478	0.6468	0.95			**
	0.1596	0.7068	0.95			
· ·	0.1105	0.7640	0.95			
* .	0.0575	0.8174	0.95	n 1		
	-0.0001		0.95			
*	-0.0625		0.95			14 14 B 14
	-0.1297		0.95			and the first of
	-0.2010		0.95		•	
	-0.2752		0.95	•	•	
	-0.3505		0.95			
	-0.4248		0.95			Election Barbara
	-0.4966		0.95			growth fire
	0.5.64.7.		0.95			
•	-0.6281	0.8719	0.95			South S
	-0.6864	0.8243	0.95			
•	-0.7397	0.7711	0.95			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
÷	-0.7882		0.95			ega Maria
	-0.8323		0.95			i Air
	-0.8726		0.95			
	-0.9095		0.95			211
	-0.9435		0.95			
	-0.9742		0.95			
	-1.0010		0.95	,		
	1.0010	0.3107	0.55			

X Inches	1:	Y Inches	Z & Span
		21101100	% Span
-1.0225		0.2446	0.95
-1.0355		0.1704	0.95
-1.0299		0.0958	0.95

[0026] In this preferred embodiment of a first stage turbine bucket, there are ninety-two (92) bucket airfoils and the state of the stat The root 31 of the bucket airfoil at the midpoint of the platform in a preferred embodiment of the turbine lies at 32.348 inches along a radius from the turbine the second and the second and the second are second as the second a centerline, i.e., rotor axis 39 (Figure 1). The actual height of the airfoil 36 in a preferred embodiment.... hereof, that is, the actual Z height of the bucket, is 7.075 inches from the root 31 at the midpoint of the platform 30 to tip 33. Thus, the tip 33 of the bucket 16 in a preferred embodiment lies 39.423 inches along a radius from the turbine centerline 39. While not forming part of the present invention, each first stage bucket airfoil 36 includes a plurality of internal air-cooling passages, not shown, which exhaust cooling air into the large are hot gas path at exit locations 42 adjacent the airfoil tip 33 as illustrated.

[0027] It will also be appreciated that the airfoil disclosed in the above Table may be scaled up or down geometrically for use in other similar turbine designs. Consequently, the coordinate values set forth in Table 1 may be scaled upwardly or downwardly such that the airfoil profile shape remains unchanged. A scaled version of the coordinates in Table I would be represented by X and Y coordinate values of Table I, and optionally the non-dimensional Z coordinate value when converted to inches, multiplied or divided by a constant number.

[0028] Referring now to Figures 9 and 10, the trailing edge of the airfoil hereof is illustrated at 50. The trailing edge of the prior known bucket is illustrated at 52. It will be appreciated from a review of Figure 8 that the trailing edge 50 has been cut back from the trailing edge 52 of the prior bucket. The cutback is indicated by the distance 54 between the trailing edges 50 and 52. The cutback extends along the entirety of the height of the trailing edge of the airfoil 36.

[0029] Referring to Figure 10, the trailing edge diameter 56 is provided in Table II below in inches at the trailing edge of the airfoil. The displacement 58 is the distance in inches that the trailing edge is reduced from the contract that the conventional bucket design previously noted. The table below thus gives the trailing edge diameters and displacements as a percentage of the span in inches of the airfoil 36. It will be appreciated that by cutting back the trailing edge configuration, an entirely new and different overall airfoil configuration is provided as compared with the prior design. For example, the trailing edge cutback results in a shorter airfoil tangent chord at each span above 0% span, i.e., the tangent chord being the linear distance between the leading edge and the trailing edge.

TABLE II

Airfoil Partial Height	TE Diameter	Displacement
0.000	0.0880	0
0.707	0.0906	0.0726
1.416	0.0885	0.1075
2.123	0.0883	0.1161

10 m	Airfoil	Salar Salar Salar	
Part	tial Height	TE Diameter	Displacement
. •			
	2.830	0.0880	0.1223
	3.538	0.0876	0.1217
	4.245	0.0870	0.1054
	4.952	0.0882	0.0822
	5.659	0.0878	0.0615
	6.368	0.0863	0.0430
ing and the second	7.075	0.0866	0.0297

[0030] While the invention has been described in connection with what is presently considered to be the most practical and preferred embodiment, it is to be understood that the invention is not to be limited to the disclosed embodiment, but on the contrary, is intended to cover various modifications and equivalent arrangements included within the spirit and scope of the appended claims.